No. 2 Recovery Furnace Maximum Emissions

Maximum production = 1,129 TBLS/day

NCASI Conversion factor = 3,500 lb BLS/ADTP

 $1,129 \text{ TBLS/day} \times 1 \text{ day/}24 \text{ hr} \times 2,000 \text{ lb/}1 \text{ ton} \times 1 \text{ ADTP/}3,500 \text{ lb BLS} = 26.88 \text{ ADTP/hr}$

Flow rate from March 31, 2010 compliance test = 114,000 dscf/min @ $7.1\% O_2$

Production during March 31, 2010 stack test = 26.76 ADTP/hr

Flow rate at maximum production = $114,000 \times 26.88 \div 26.76 = 114,500 \text{ dscf/min}$

Particulate Matter (PM)

MACT Emission limit = 0.044 gr/dscf @ 8% O₂

 $0.044 \text{ gr/dscf} \times (20.9 - 7.1) / (20.9 - 8) = 0.047 \text{ gr/dscf}$

 $0.047 \text{ gr/dscf} \times 114,500 \text{ dscf/min} \times 60 \text{ min/hr} \times 1 \text{ lb/7,000 gr} = 46.13 \text{ lb/hr}$

 $46.13 \text{ lb/hr} \times 8,760 \text{ hr/yr} \times 1 \text{ ton/2,000 lb} = 202 \text{ tons/yr}$

Total Reduced Sulfur (TRS as H₂S)

State Allowable emission limit = 20 ppm @ 8% O₂

 $20 \text{ ppm} \times (20.9 - 7.1)/(20.9 - 8) = 21.4 \text{ ppm}$

 $21.4 \text{ ppm} \times 34/385.3\text{E}6 \times 114,500 \text{ dscf/min} \times 60 \text{ min/hr} = 13.0 \text{ lb/hr}$

 $13.0 \text{ lb/hr} \times 8,760 \text{ hr/yr} \times 1 \text{ ton/2,000 lb} = 56.9 \text{ tons/yr}$

No. 3 Recovery Furnace Maximum Total Reduced Sulfur (TRS as H2S) Emissions

Maximum production = 2,040 TBLS/day

Flow rate from December 2, 2003 compliance test = 183,000 dscf/min @ 5.5% O₂

Production during December 2, 2003 stack test = 73.5 TBLS/hr = 1,764 TBLS/day

Flow rate at maximum production = $183,000 \times 2,040 \div 1,764 = 211,600$ dscf/min

BACT/NSPS emission limit = 5 ppm @ 8% O₂

 $5 \text{ ppm} \times (20.9 - 5.5)/(20.9 - 8) = 5.969 \text{ ppm}$

 $5.969~ppm \times 34/385.3E6 \times 211,\!600~dscf\!/min \times 60~min\!/hr = 6.69~lb\!/hr$

6.69 lb/hr \times 8,760 hr/yr \times 1 ton/2,000 lb = 29.3 tons/yr

No. 2 Lime Kiln Maximum Nitrogen Oxide (NOx) Emissions

2001 PSD BACT emission limit = 152 ppm @ 10% O₂

Flow rate from October 22, 1999 stack test (PM) = 21,900 dscf/min @ 2.7% O₂

Production rate during October 22, 1999 stack test (PM) = 340 tons CaO/day

Flow rate at maximum production = $21,900 \text{ dscf/min} \times 465 \text{ tons CaO/day} \div 340 \text{ tons CaO/day}$ = 30,000 dscf/min

 $152 \text{ ppm} \times (20.9 - 2.7) / (20.9 - 10) = 254 \text{ ppm}$

254 ppm \times 46/385.3E6 \times 30,000 dscf/min \times 60 min/hr = 54.5 lb/hr

 $54.5 \text{ lb/hr} \times 8,760 \text{ hr/yr} \times 1 \text{ ton/2,000 lb} = 239 \text{ tons/yr}$

Fresh Lime Silo and Reburn Lime Silo Particulate Matter (PM) Emissions

Emission factor from 1994 permit application = 0.02 gr/acf

Flow rate from 1994 permit application = 3,835 acfm

 $0.02 \text{ gr/acf} \times 3,835 \text{ acf/min} \times 60 \text{ min/hr} \times 1 \text{ lb/7,000 gr} = 0.66 \text{ lb/hr maximum}$

Assume actual = $0.5 \times \text{maximum} = 0.5 \times 0.66 = 0.33 \text{ lb/hr actual}$

No. 3 Recovery Furnace Emission Factors (2005 PSD/NSR Permit)

Particulate Matter (PM)

NCASI TB 884 emission factors = 0.37 lb/TBLS (filterable)

= 0.063 lb/TBLS (condensable)

December 2, 2003 compliance test = $29.4 \text{ lb/hr} \times \text{hr}/73.5 \text{ TBLS} = 0.40 \text{ lb/TBLS}$ (filterable)

August 4, 2004 compliance test = 23 lb/hr \times hr/68 TBLS = 0.34 lb/TBLS (filterable)

February 15, 2005 engineering test = $48.7 \text{ lb/hr} \times \text{hr/}66.3 \text{ TBLS} = 0.73 \text{ lb/TBLS}$ (filterable)

February 16, 2005 engineering test = $45.4 \text{ lb/hr} \times \text{hr/}69.7 \text{ TBLS} = 0.65 \text{ lb/TBLS}$ (filterable)

Average test value = $[0.40 + 0.34 + 0.73 + 0.65] \div 4 = 0.53 \ lb/TBLS$ (filterable)

Sulfur Dioxide (SO₂)

NCASI TB 884 emission factor = 0.22 lb/TBLS

December 2, 2003 compliance test = $17.7 \text{ lb/hr} \times \text{hr}/73.5 \text{ TBLS} = 0.24 \text{ lb/TBLS}$

August 4, 2004 compliance test = $2.1 \text{ lb/hr} \times \text{hr/}68 \text{ TBLS} = 0.031 \text{ lb/TBLS}$

Average test value = $[0.24 + 0.031] \div 2 = 0.14 \text{ lb/TBLS}$

Nitrogen Oxide (NO_X)

NCASI TB 884 emission factor = 1.50 lb/TBLS

December 2, 2003 compliance test = $108.5 \text{ lb/hr} \times \text{hr}/73.5 \text{ TBLS} = 1.48 \text{ lb/TBLS}$

August 4, 2004 compliance test = $86.7 \text{ lb/hr} \times \text{hr/}68 \text{ TBLS} = 1.28 \text{ lb/TBLS}$

Average test value = $[1.48 + 1.28] \div 2 = 1.38 \text{ lb/TBLS}$

Carbon Monoxide (CO)

NCASI TB 884 emission factor = 1.21 lb/TBLS

December 2, 2003 compliance test = $65.2 \text{ lb/hr} \times \text{hr}/73.5 \text{ TBLS} = 0.89 \text{ lb/TBLS}$

August 4, 2004 compliance test = $109 \text{ lb/hr} \times \text{hr/}68 \text{ TBLS} = 1.60 \text{ lb/TBLS}$

Average test value = $[0.89 + 1.60] \div 2 = 1.25 \ lb/TBLS$

No. 2 Lime Kiln Emission Factors (2005 PSD/NSR Permit)

Particulate Matter (PM)

NCASI TB 884 emission factor = 0.089 lb/ton CaO (filterable)

= 0.188 lb/ton CaO (condensable)

December 2, 2003 compliance test = $2.1 \text{ lb/hr} \times \text{hr/}17 \text{ ton CaO} = 0.12 \text{ lb/ton CaO}$ (filterable)

August 4, 2004 compliance test = $2.1 \text{ lb/hr} \times \text{hr}/16.6 \text{ ton CaO} = 0.13 \text{ lb/ton CaO}$ (filterable)

Average test value = $[0.12 + 0.13] \div 2 = 0.125 \text{ lb/ton CaO (filterable)}$

Sulfur Dioxide (SO₂)

NCASI TB 884 emission factor = 0.33 lb/ton CaO

December 2, 2003 compliance test = $0.33 \text{ lb/hr} \times \text{hr/}17 \text{ ton CaO} = 0.019 \text{ lb/ton CaO}$

August 4, 2004 compliance test = $0.28 \text{ lb/hr} \times \text{hr}/16.6 \text{ ton CaO} = 0.017 \text{ lb/ton CaO}$

Average test value = $[0.019 + 0.017] \div 2 = 0.018$ lb/ton CaO

Nitrogen Oxide (NO_X)

NCASI TB 884 emission factor = 1.15 lb/ton CaO

December 2, 2003 compliance test = $47.1 \text{ lb/hr} \times \text{hr}/17 \text{ ton CaO} = 2.77 \text{ lb/ton CaO}$

August 4, 2004 compliance test = $24.4 \text{ lb/hr} \times \text{hr}/16.6 \text{ ton CaO} = 1.47 \text{ lb/ton CaO}$

Average test value = $[2.77 + 1.47] \div 2 = 2.12 \ lb/ton \ CaO$

Carbon Monoxide (CO)

NCASI TB 884 emission factor = 0.055 lb/ton CaO

December 2, 2003 compliance test = $2.8 \text{ lb/hr} \times \text{hr/}17 \text{ ton CaO} = 0.165 \text{ lb/ton CaO}$

August 4, 2004 compliance test = $1.5 \text{ lb/hr} \times \text{hr}/16.6 \text{ ton CaO} = 0.090 \text{ lb/ton CaO}$

Average test value = $[0.165 + 0.090] \div 2 = 0.128 \ lb/ton \ CaO$